

### STATE OF CONNECTICUT

### CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051 Phone: (860) 827-2935 Fax: (860) 827-2950 E-Mail: siting.council@ct.gov www.ct.gov/csc

December 11, 2008

Carrie L. Larson, Esq. Pullman & Comley, LLC 90 State House Square Hartford, CT 06103-3702

RE:

**EM-POCKET-002-081110** – Youghiogheny Communications-Northeast, LLC d/b/a Pocket Communications notice of intent to modify an existing telecommunications facility located at 1 Deerfield Lane, Ansonia, Connecticut.

Dear Attorney Larson:

The Connecticut Siting Council (Council) hereby acknowledges your notice to modify this existing telecommunications facility, pursuant to Section 16-50j-73 of the Regulations of Connecticut State Agencies.

The proposed modifications are to be implemented as specified here and in your notice dated November 7, 2008, including the placement of all necessary equipment and shelters within the tower compound. The modifications are in compliance with the exception criteria in Section 16-50j-72 (b) of the Regulations of Connecticut State Agencies as changes to an existing facility site that would not increase tower height, extend the boundaries of the tower site, increase noise levels at the tower site boundary by six decibels, and increase the total radio frequencies electromagnetic radiation power density measured at the tower site boundary to or above the standard adopted by the State Department of Environmental Protection pursuant to General Statutes § 22a-162. This facility has also been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequencies now used on this tower.

This decision is under the exclusive jurisdiction of the Council. Please be advised that the validity of this action shall expire one year from the date of this letter. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Any deviation from this format may result in the Council implementing enforcement proceedings pursuant to General Statutes § 16-50u including, without limitation, imposition of expenses resulting from such failure and of civil penalties in an amount not less than one thousand dollars per day for each day of construction or operation in material violation.

Thank you for your attention and cooperation.

S. Derek Phelps

SDP/CDM/laf

c: The Honorable James T. DellaVolpe, Mayor, City of Ansonia Peter Crabtree, Zoning Enforcement Officer, City of Ansonia SBA



## Daniel F. Caruso Chairman

### STATE OF CONNECTICUT

CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051 Phone: (860) 827-2935 Fax: (860) 827-2950 E-Mail: siting.council@ct.gov Internet: ct.gov/csc

November 14, 2008

The Honorable James T. DellaVolpe Mayor City of Ansonia City Hall 253 Main Street Ansonia, CT 06401-1866

RE:

EM-POCKET-002-081110 – Youghiogheny Communications-Northeast, LLC d/b/a Pocket Communications notice of intent to modify an existing telecommunications facility located at 1 Deerfield Lane, Ansonia, Connecticut.

Dear Mayor DellaVolpe:

The Connecticut Siting Council (Council) received this request to modify an existing telecommunications facility, pursuant to Regulations of Connecticut State Agencies Section 16-50j-72.

If you have any questions or comments regarding this proposal, please call me or inform the Council by November 28, 2008.

Thank you for your cooperation and consideration.

IX/ NA

Executive Director

SDP/jb

Very tru

Enclosure: Notice of Intent

c: Peter Crabtree, Zoning Enforcement Officer, City of Ansonia



EM-POCKET-002-081110

CARRIE L. LARSON
90 State House Square
Hartford, CT 06103-3702
p (860) 424-4312
f (860) 424-4370

ORIGINAL

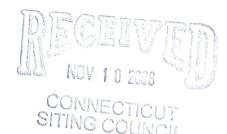
www.pullcom.com

November 7, 2008

1

Via Federal Express

S. Derek Phelps, Executive Director Connecticut Siting Council Ten Franklin Square New Britain, CT 06051



**Re:** Notice of Exempt Modification

SBA Infrastructure, LLC (formerly known as Optasite)

**Telecommunications Facility** 

1 Deerfield Lane, Ansonia, Connecticut

Dear Mr. Phelps:

Youghiogheny Communications-Northeast, LLC. doing business **Pocket** Communications ("Pocket"), intends to install antennas and appurtenant equipment at the existing 170-foot monopole facility owned by SBA Infrastructure, LLC (formerly known as Optasite) and located at 1 Deerfield Lane, Ansonia, Connecticut, Connecticut ("Facility"). Pocket Communications provides prepaid, flat rate wireless voice and data services to more than a quarter of a million subscribers. Pocket is licensed by the Federal Communications Commission (FCC) to provide PCS wireless telecommunications service in the State of Connecticut, which includes the area to be served by the proposed installation. This installation constitutes an exempt modification pursuant to the Public Utility Environmental Standards Act, Connecticut General Statutes Section 16-50g et. seq. (PUESA), and Section 16-50j-72(b)(2) of the Regulations of the Connecticut State Agencies adopted pursuant to PUESA. In accordance with R.C.S.A. Section 16-50j-73, a copy of this notice has been sent to James T. Della Volpe, Mayor, City of Ansonia.

The existing Facility consists of a 170-foot self-supporting monopole tower capable of supporting multiple carriers within a fenced compound. The coordinates for the Facility are Lat: 41°-21'-2.7" and Long: 73°-2'-57.3". The tower is located on a former Nike missile site, on the eastern edge of Ansonia, roughly 3,000 feet southwest of Rimmon Road (Route 319) in Woodbridge. The Facility stands roughly one mile to the northeast of the downtown area of Ansonia (see Site Map, attached as Exhibit A). The tower currently supports AT&T antennas at the one hundred forty seven foot (147') level centerline AGL (above ground level), Verizon antennas at the one hundred fifty seven foot level (157') AGL, and T-Mobile antennas at the one hundred sixty seven foot level (167') AGL. Pocket proposes to install three RFS APXV18-206517S-C flush mount antennas on the tower at the one hundred thirty seven foot centerline

## PULLMAN & COMLEY, LLC ATTORNEYS AT LAW

Page 2

(137') AGL, and a Nortel CDMA Micro BTS 3231 cabinet, mounted on an "H-Frame," contained within a six foot by six foot (6'-0" x 6'-0") lease area. A small GPS antenna will be mounted to the H-Frame. An ice bridge will run from the lease area to the tower. Utilities will be run via a proposed underground conduit from an existing utility backboard, within the compound (See Design Drawings and Equipment Specifications, attached as Exhibits B and C respectively).

For the following reasons, the proposed modifications to the Deerfield Lane Facility meet the exempt modification criteria set forth in R.C.S.A. Section 16-50j-72(b)(2):

- 1. The proposed modification will not increase the height of the tower as Pocket's antennas will be installed at a center line height of approximately 137 feet.
- 2. The installation of Pocket's equipment and shelter will not require an extension of the site boundaries.
- 3. The proposed modifications will not increase the noise levels at the existing Facility by six decibels or more.
- 4. The operation of the additional antennas will not increase the total radio frequency (RF) power density, measured at the site boundary, to a level at or above the standard adopted by the Connecticut Department of Environmental Protection as set forth in Section 22a-162 of the Connecticut General Statutes and MPE limits established by the Federal Communications Commission. The worst-case RF power density calculations for the proposed Pocket antennas would be 17.08% of the FCC standard (see general power density calculations table, attached as Exhibit D).

Also attached, Exhibit E, is a structural analysis confirming that the tower can support the existing and proposed antennas and associated equipment.

For the foregoing reasons, Pocket respectfully submits that the proposed antenna installation and equipment at the Ansonia Facility constitutes an exempt modification under R.C.S.A. Section 16-50j-72(b)(2)

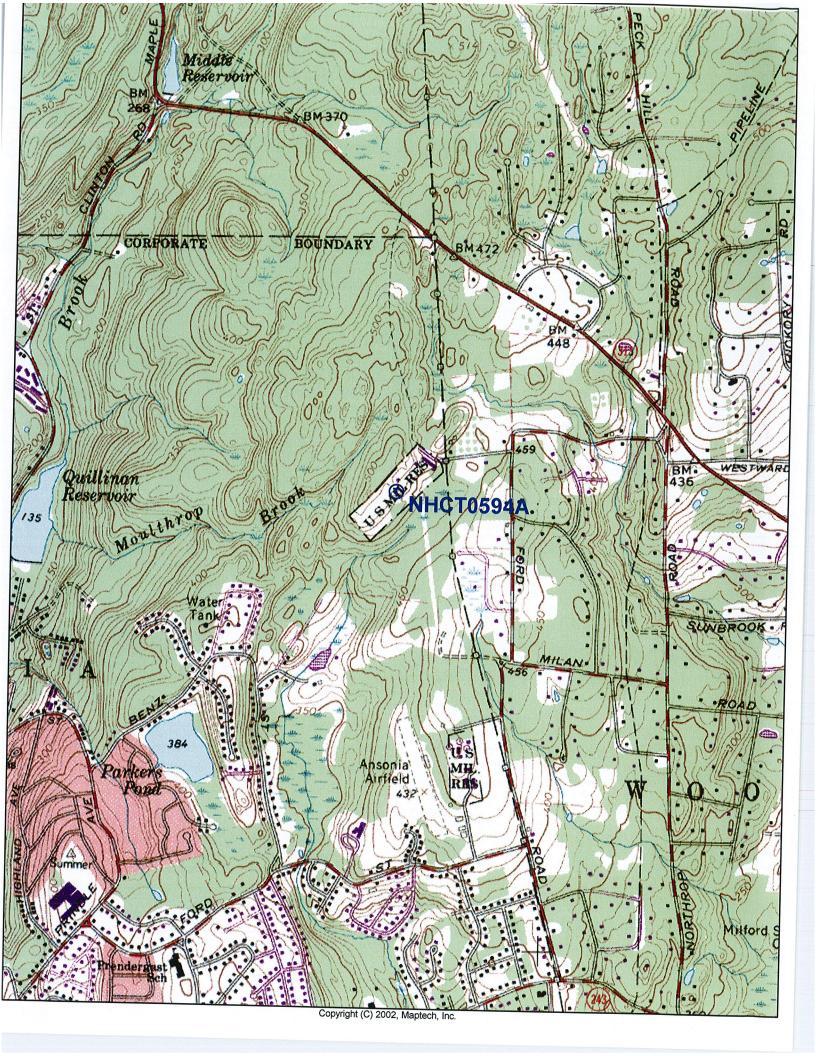
Respectfully Submitted,

Carrie L. Larson

cc: James T. Della Volpe, Mayor, City of Ansonia Macabee Properties, LLC, Attn: Joel & Cheryl Gelernter, underlying property owners

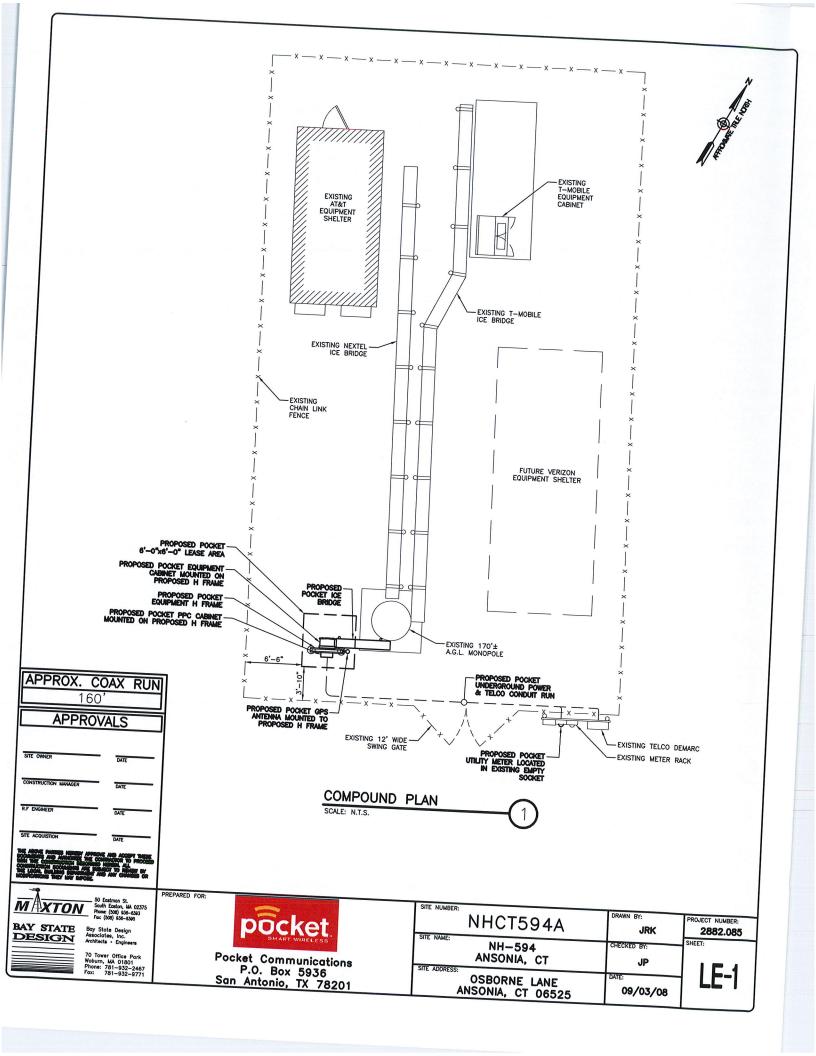
## Exhibit A

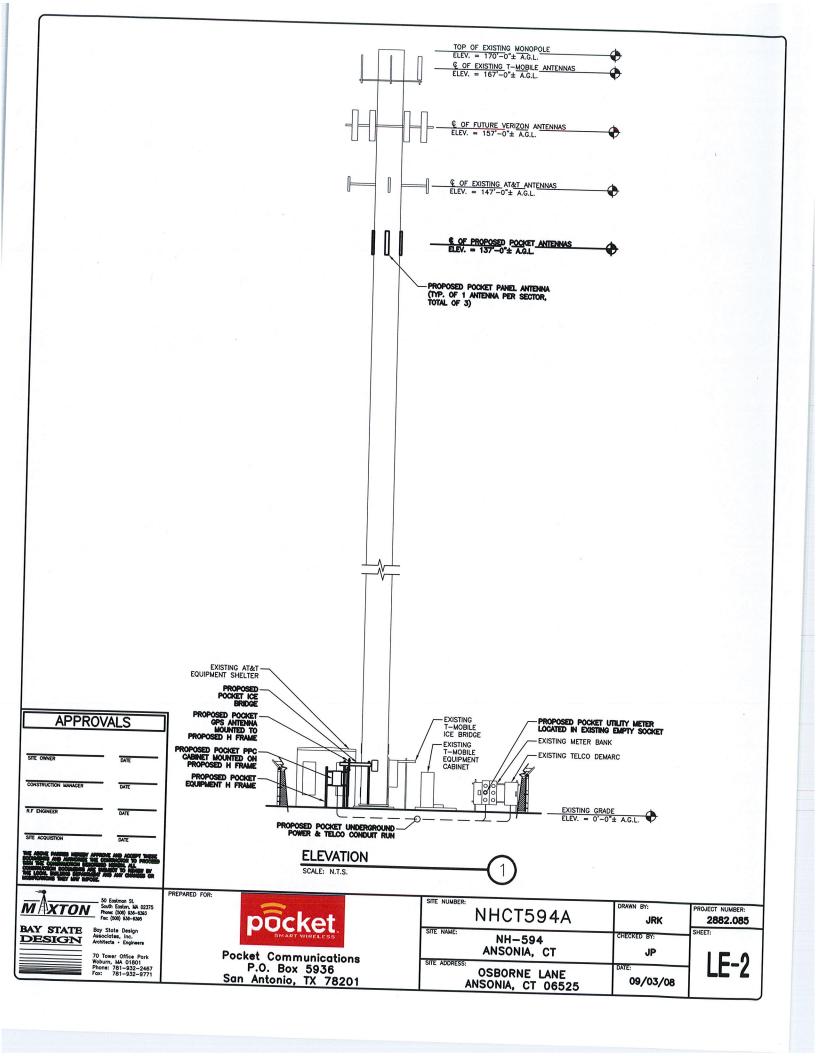
## Site Map Pocket Site NHCT0594A 1 Deerfield Lane Ansonia, Connecticut



## Exhibit B

# Design Drawings Pocket Site NHCT0594A 1 Deerfield Lane Ansonia, Connecticut





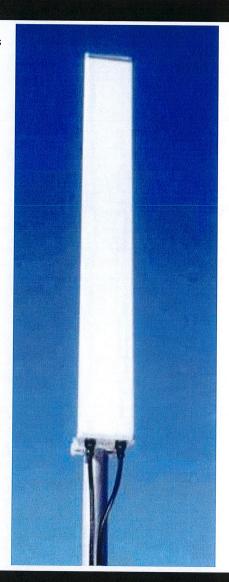
## Exhibit C

## Equipment Specifications Pocket Site NHCT0594A 1 Deerfield Lane Ansonia, Connecticut



### **Product Description**

This variable tilt antenna provides exceptional suppression of all upper sidelobes at all downtilt angles. It also features null fill and a wide downtilt range with optional remote tilt.



### Features/Benefits

- $\bullet$  Variable electrical downtilt provides enhanced precision in controlling intercell interference. The tilt is infield adjustable 0-10 deg.
- High Suppression of all Upper Sidelobes (Typically <-20dB).
- Optional remote tilt can be retrofitted.
- Broadband design.
- Dual polarization.
- Low profile for low visual impact.

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CC		(.a		alli	11 25

Frequency Band	3G/UMTS (Single, Broad, Dual and Triple-Band)
Horizontal Pattern	Directional
Antenna Type	Panel Dual Polarized
Electrical Down Tilt Option	Variable

RFS The Clear Choice ™

APXV18-206517S-C

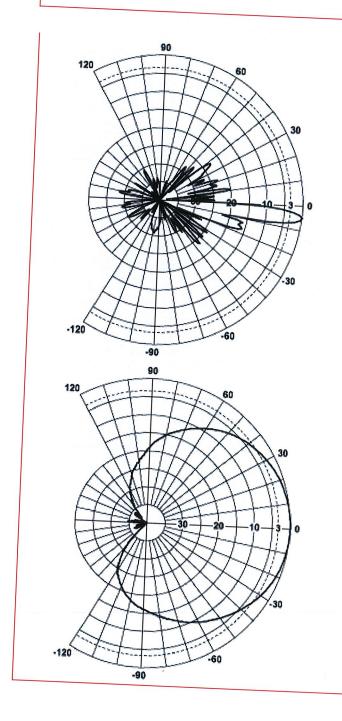
Print Date: 02.09.2008

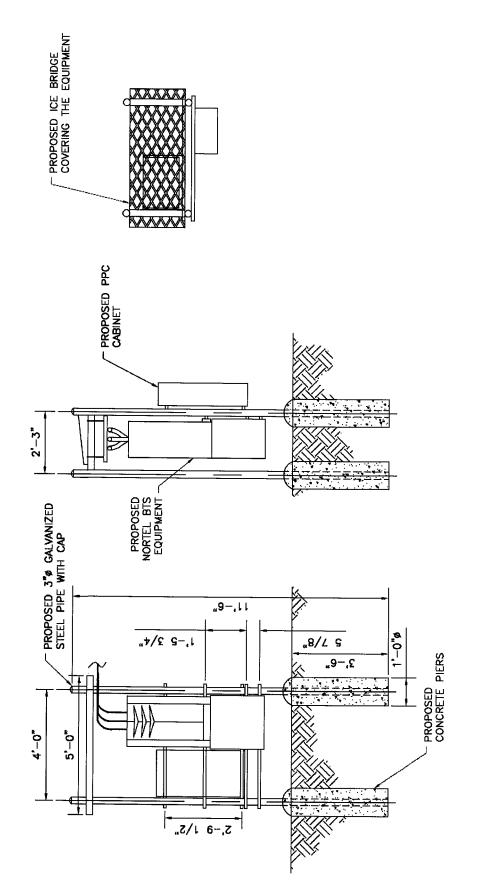


Gain, dBi (dBd)	18.8 (16.7) , 19.0 (16.9)
Frequency Range, MHz	1710-1900, 1900-2170
Connector Type	(2) 7-16 DIN Female
Connector Location	Bottom
Mount Type	Downtilt
Electrical Downtilt, deg	0-10
Horizontal Beamwidth, deg	67 , 63
Mounting Hardware	APM40-2
Rated Wind Speed, km/h (mph)	160 (100)
VSWR	< 1.5:1
Vertical Beamwidth, deg	5.0 , 4.6
Upper Sidelobe Suppression, dB	>17 , >18 all (Typically >20)
Polarization	Dual pol +/-45°
Front-To-Back Ratio, dB	>30
Maximum Power Input, W	300
Isolation between Ports, dB	>30
Lightning Protection	Direct Ground
3rd Order IMP @ 2 x 43 dBm, dBc	>150
7th Order IMP @ 2x46 dBm, dBc	>170
Impedance, Ohms	50
Overall Length, m (ft)	1.85 (6.06)
Mounting Hardware Weight, kg (lb)	3.4 (7.5)
Dimensions - HxWxD, mm (in)	1850 x 175 x 80 (72.0 x 6.8 x 3.15)
Weight w/o Mtg Hardware, kg (lb)	12 (26.4)
Weight w/ Mtg Hardware, kg (lb)	14.8 (32.5)
Radiating Element Material	Brass
Radome Color	Light Grey RAL7035
Radome Material	Fiberglass
Mounting Hardware Material	Diecasted Aluminum
Reflector Material	Aluminum
Max Wind Loading Area, m² (ft²)	0.31 (3.3)
Survival Wind Speed, km/h (mph)	200 (125)
Maximum Thrust @ Rated Wind, N (lbf)	558 (125)
Front Thrust @ Rated Wind, N (lbf)	558 (125)
Shipping Weight, kg (lb)	18.3 (39.8)
Packing Dimensions, HxWxD, mm (in)	2021 x 260 x 200 (79.5 x 10.2 x 7.8)

DEC	The	Class	Chaica	TM







Pocket/Youghiogheny Communications – Northeast, LLC Rack Detail



### >BUSINESS MADE SIMPLE



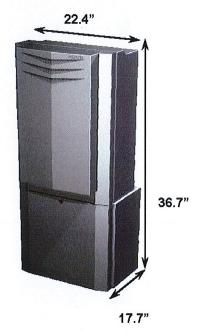
### CDMA BTS 3231 AWS 1.7/2.1 GHz (Outdoor/Indoor)

**CDMA BTS 3231** 

### Industry's Highest Capacity AWS Micro BTS

The CDMA BTS 3231 is the latest extension to Nortel Networks BTS (Base Transceiver Station) portfolio providing the ideal solution for urban, sub-urban and rural deployments. The CDMA BTS 3231 is a 3-carrier, 3-sector outdoor/indoor BTS operating at the AWS band of 1.7/2.1 GHz supporting IS-95, 1XRTT and 1xEV-DO simultaneously. BTS 3231 provides flexible deployments solutions including floor, rack, and wall mount options. The power consumption of BTS3231 is industry leading consuming only 630W for 3C3S. The BTS 3231 is also very light at 240lbs making it easy

to transport to hard to reach locations such as the top of a high rise building.



## Exhibit D

## Power Density Calculations Pocket Site NHCT0594A 1 Deerfield Lane Ansonia, Connecticut



C Squared Systems, LLC 920 Candia Road Manchester, NH 03109 Phone: (603) 657 9702 E-mail:

support@csquaredsystems.com

### Calculated Radio Frequency Emissions



**NHCT0594** 

1 Deerfield Lane, Ansonia, CT

### **Table of Contents**

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2. FCC Guidelines for Evaluating RF Radiation Exposure Limits
3. RF Exposure Prediction Methods
4. Calculation Results
5. Conclusion
6. Statement of Certification
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Attachment B: FCC Limits For Maximum Permissible Exposure (MPE)
List of Tables
Table 1: Proposed Carrier Information

### 1. Introduction

The purpose of this report is to investigate compliance with applicable FCC regulations for the proposed Pocket antennas to be installed on the existing tower at 1 Deerfield Lane, Ansonia, CT.

These calculations assume that the antennas are operating at 100 percent capacity, that all antenna channels are transmitting simultaneously, and that the radio transmitters are operating at full power. Obstructions (trees, buildings etc.) that would normally attenuate the signal are not taken into account. As a result, the predicted signal levels are much more conservative (higher) than the actual signal levels will be from the finished installation.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter (mW/cm²). The number of mW/cm² emitted is called the power density. The general population exposure limit for the cellular band is 0.567-0.593 mW/cm², and the general population exposure limit for the PCS/AWS band is 1.0 mW/cm². Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

The FCC general population / uncontrolled limits set the maximum exposure to which most people may be subjected. General population / uncontrolled exposures apply in situations in which the general public may be exposed, or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over their exposure.

Higher exposure limits are permitted under the occupational / controlled exposure category, but only for persons who are exposed as a consequence of their employment and who have been made fully aware of the potential for exposure (through training), and they must be able to exercise control over their exposure. General population / uncontrolled limits are five times more stringent than the levels that are acceptable for occupational, or radio frequency trained individuals."

The FCC describes exposure to radio frequency (RF) energy in terms of percentage of maximum permissible exposure (MPE) with 100% being the maximum allowed. Rather than the FCC presenting the user specification in terms of complex power density figures over a specified surface area, this MPE measure is particularly useful, and even more so when considering that power density limits actually vary by frequency because of the different absorptive properties of the human body at different frequencies.

MPE limits are specified as time-averaged exposure limits. This means that exposure can be averaged over 30 minutes for general population / uncontrolled exposure (or 6 minutes for occupational / controlled exposure). However, for the case of exposure of the general public, time averaging is usually not applied because of uncertainties over exact exposure conditions and difficulty in controlling time of exposure. Therefore, the typical conservative approach is to assume that any RF exposure to the general public will be continuous.

Finally, it should be noted that the MPE limits adopted by the FCC for both general population / uncontrolled exposure and for occupational / controlled exposure incorporate a substantial margin of safety and have been established to be well below levels generally accepted as having the potential to cause adverse health effects.

### 2. FCC Guidelines for Evaluating RF Radiation Exposure Limits

In 1985, the FCC established rules to regulate radio frequency (RF) exposure from FCC licensed antenna facilities. In 1996, the FCC updated these rules, which were further amended in August 1997 by OET Bulletin 65 Edition 97-01. These new rules include limits for Maximum Permissible Exposure (MPE) for transmitters operating between 300 kHz and 100 GHz. The FCC MPE limits are based on exposure limits recommended by the National Council on Radiation Protection and Measurements (NCRP), the exposure limits developed by the Institute of Electrical and Electronics Engineers, Inc., (IEEE) and adopted by the American National Standards Institute (ANSI).

Attachment B contains excerpts from OET Bulletin 65 and defines the Maximum Exposure Limit. As shown in these excerpts, each frequency band has different exposure limits, requiring power density to be reported as a percent of Maximum Permissible Exposure (MPE) when dealing with carriers transmitting in different frequency bands.

### 3. RF Exposure Prediction Methods

The emission field calculation results displayed in the following figures were generated using the following formula as outlined in FCC bulletin OET 65:

Power Density = 
$$\left(\frac{EIRP}{\pi \times R^2}\right) \times \text{Off Beam Loss}$$

Where:

EIRP = Effective Isotropic Radiated Power

 $R = Radial Distance = \sqrt{(H^2 + V^2)}$ 

H = Horizontal Distance from antenna

V = Vertical Distance from bottom of antenna

Off Beam Loss is determined by the selected antenna patterns

### 4. Calculation Results

Table 1 below outlines the power density information for the site. All information for carriers other than Pocket was obtained from previous siting council filings.

Carrier	Number of Trans.	Effective Radiated Power (ERP) Per Transmitter (Watts)	Antenna Height (Feet)	Operating Frequency (MHz)	Total ERP (Watts)	Power Density (mw/cm^2)	Limit	%МРЕ
T-Mobile	8	142	167	1945	1,136	0.0146	1.0000	1.46%
Verizon cellular	9	200	157	880	1,800	0.0263	0.5867	4.48%
Verizon PCS	6	200	157	1970	1,200	0.0175	1.0000	1.75%
AT&T GSM	2	296	147	1900	592	0.0099	1.0000	0.99%
AT&T GSM	4	296	147	880	1,184	0.0197	0.5867	3.36%
AT&T UMTS	1	500	147	880	500	0.0083	0.5867	1.42%
Pocket	3	631	137	2130- 2133.75	1,893	0.0363	1.0000	3.63%
				20110			Total	17.08%

**Table 1: Proposed Carrier Information** 

### 5. Conclusion

The above analysis verifies that emissions from the proposed site will be well below the maximum power density levels as outlined by the FCC in the OET Bulletin 65 Ed. 97-01. Even when using conservative methods, the cumulative power density from the proposed transmit antennas at the existing facility is well below the limits for the general public. The highest expected percent of Maximum Permissible Exposure at the base of the tower is 17.08% of the FCC limit.

As noted in the introduction, obstructions (trees, buildings etc.) that would normally attenuate the signal are not taken into account. As a result, the predicted signal levels are more conservative (higher) than the actual signal levels will be from the finished installation.

### 6. Statement of Certification

I certify to the best of my knowledge that the statements in this report are true and accurate. The calculations follow guidelines set forth in ANSI/IEEE Std. C95.3, ANSI/IEE Std. C95.1 and FCC OET Bulletin 65 Edition 97-01.

Tony Wells

C Squared Systems

September 7, 2008

Date

### **Attachment A: References**

OET Bulletin 65 - Edition 97-01 - August 1997 Federal Communications Commission Office of Engineering & Technology

ANSI C95.1-1982, American National Standard Safety Levels With Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 300 kHz to 100 GHz. IEEE-SA Standards Board

IEEE Std C95.3-1991 (Reaff 1997), IEEE Recommended Practice for the Measurement of Potentially Hazardous Electromagnetic Fields - RF and Microwave. IEEE-SA Standards Board

### Attachment B: FCC Limits For Maximum Permissible Exposure (MPE)

### (A) Limits for Occupational/Controlled Exposure

Frequency	Electric Field	Magnetic Field	Power Density (S)	Averaging Time
Range	Strength (E)	Strength (E)	= 0 11 22 elliolety (8)	$ E ^2$ , $ H ^2$ or S
(MHz)	(V/m)	(A/m)	$(mW/cm^2)$	(minutes)
0.3-3.0	614	1.63	(100)*	6
3.0-30	1842/f	4.89/f	$(900/f^2)*$	6
30-300	61.4	0.163	1.0	6
300-1500	<del>-</del>	-	f/300	6
1500-100,000	-	-	5	6

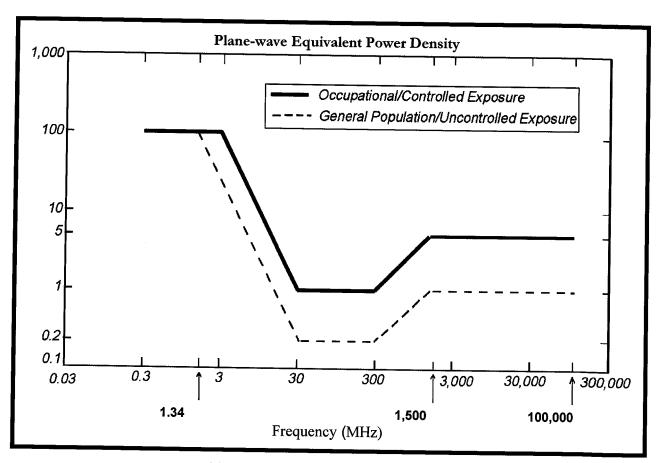
### (B) Limits for General Population/Uncontrolled Exposure

Frequency	Electric Field	Magnetic Field	Power Density	Averaging Time
Range	Strength (E)	Strength (E)	(S)	$ E ^2$ , $ H ^2$ or S
(MHz)	(V/m)	(A/m)	$(mW/cm^2)$	(minutes)
0.3-1.34	614	1.63	(100)*	30
1.34-30	824/f	2.19/f	$(180/f^2)*$	30
30-300	27.5	0.073	0.2	30
300-1500	-	_	f/1500	30
1500-100,000	-	-	1.0	30

f = frequency in MHz \* Plane-wave equivalent power density

NOTE 1: Occupational/controlled limits apply in situations in which persons are exposed as a consequence of their employment provided those persons are fully aware of the potential for exposure and can exercise control over their exposure. Limits for occupational/controlled exposure also apply in situations when an individual is transient through a location where occupational/controlled limits apply provided he or she is made aware of the potential for exposure.

NOTE 2: General population/uncontrolled exposures apply in situations in which the general public may be exposed, or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or can not exercise control over their exposure.



• FCC Limits for Maximum Permissible Exposure (MPE)

## Exhibit E

## Structural Analysis Pocket Site NHCT0594A 1 Deerfield Lane Ansonia, Connecticut

### Structural Analysis Report

Job Number: 09-10359

Existing 170' Sabre Communications Corporation 18-sided Monopole

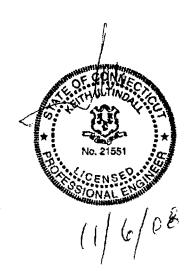
Located at Ansonia, CT

Report Completed for

Bay State Design Inc.

Woburn, MA

Prepared by
Sabre Towers & Poles
November 5, 2008



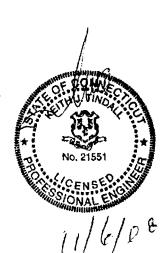
## Structural Analysis Report Existing 170' Sabre Communications Corporation 18-sided Monopole

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METHOD OF ANALYSIS	
SUPPORTED EQUIPMENT	
RESULTS	
CONCLUSIONS	
DESCRIPTION OF MONOPOLE PROGRAM	
PLOTS & CALCULATIONS	

Prepared by KIT

Approved by KIT



### Introduction

The purpose of this analysis is to determine if the existing tower is in conformance with the requirements of ANSI/TIA-222-G, while supporting specified equipment. The tower is a 170' 18-sided monopole and was originally manufactured by Sabre Communications Corporation. The tower is located in Ansonia, CT. The analysis is being performed for Bay State Design

### **Method of Analysis**

The computer program that was used for this analysis is described on the attached page. The analysis was performed using a basic wind speed of 110 with no ice and 50 with 0.75" ice, in accordance with ANSI/TIA-222-G. Factored resistances and load factors were also determined in accordance with

### Supported Equipment

The analysis was performed for the tower, supporting the following equipment:

- 1. Nine (9) APXV18-209014-C antennas on three (3) T-Arms at 167', with eighteen (18) 1-5/8" lines
- 2. Three (3) TMA's on the same mounts as above at 167'
- 3. Twelve (12) LPA-185063/8CF antennas on three (3) T-Arms at 157', with fifteen (15) 1-5/8" lines
- 4. Six (6) 7770 antennas on three (3) T-Arms at 147', with twelve (12) 1-5/8" lines
- 5. Six (6) TMA's on the same mounts as above at 147'
- 6. Six (6) diplexers on the same mounts as above at 147'
- 7. Three (3) APXV18-206517-C antennas at 137', with six (6) 1-5/8" lines

The transmission lines are assumed to run inside the pole.

### Results

The results of the analysis show no overloads in any tower component.

The maximum utilization ratio in any tower component is 77%.

In addition, the results of the analysis show that the foundations are adequate.

### Conclusions

Based on the preceding results, the following conclusions have been made:

- 1. The tower with specified equipment is adequate to achieve a basic wind speed rating of 110 mph with no ice and 50 mph with 0.75" ice, in accordance with ANSI/TIA-222-G.
- 2. No modifications are required, in order to meet the structural criteria stated above.
- 3. The analysis is valid only for the equipment listed above. If the equipment is not as listed, an additional analysis should be performed.
- 4. The analysis assumes that the tower contains no structural defects, and that all components have been installed properly.

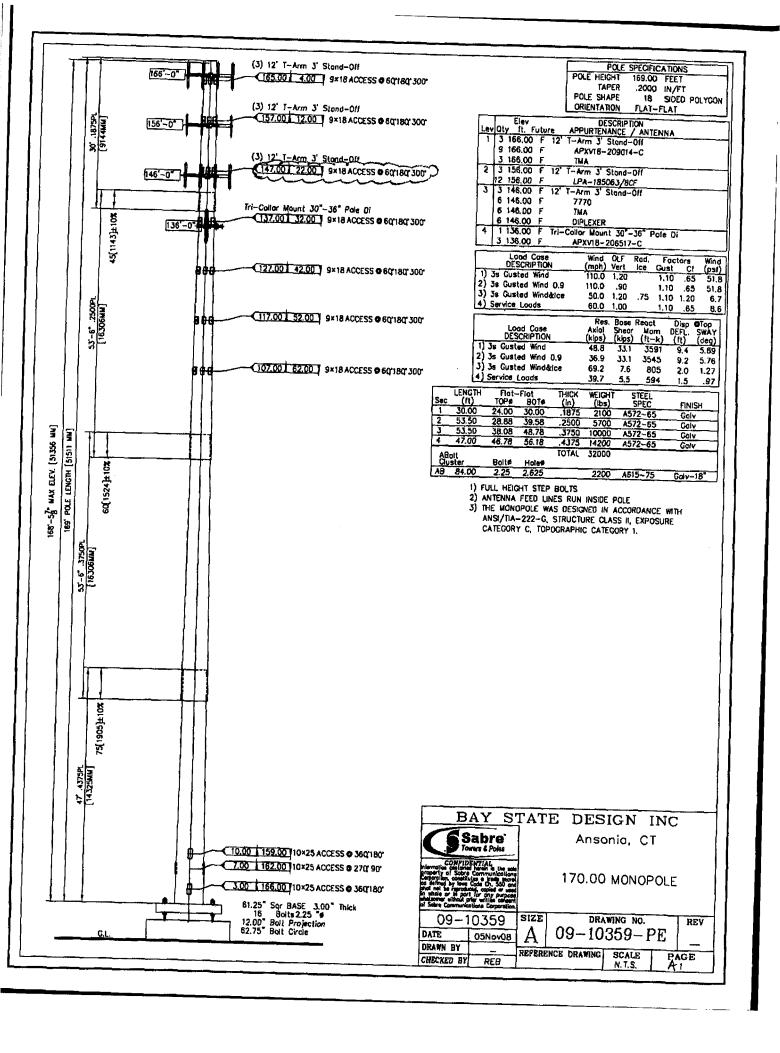
### Description of Monopole Computer Program

A customized monopole computer program is utilized by Sabre Communications to perform the structural analysis and design of monopoles.

The basic criteria for designing a monopole such as wind speed, effective areas of monopole sections, factored resistances, allowable rigidity and foundation requirements are based on ANSI/TIA Standard 222-G.

A monopole is treated as a cantilevered beam with a fixed base support. Wind, ice and weight are the major design loads considered in the static analysis. Effects due to eccentric moments, torques, slopes and deflections are included in the computer program.

After all the necessary input data is entered, the program will compute the effective area of each monopole section, the wind loads at each elevation, and the factored resistance of each section. The total weight, wind shear, overturning moment and torque are calculated at each elevation, in order to determine loads in each section of the monopole. The factored loads are then compared with the factored resistances to determine the adequacy and/or required sizes.



SABRE COMMUNICATIONS CORP 2101 Murray Street JOB: 09-10359 05-Nov-08 15:38 BAY STATE DESIGN INC Sioux City, IA 51101 Ph 712.258.6690 Ansonia, CT Fx 712.258.8250 DIAMETER

TOP BOTTOM 24.00 in. [ 24.37 in. Point-Point] 56.18 in. [ 57.04 in. Point-Point] 169.00 ft. 18 SIDED FLAT ORIENTA 1.00 ft. ABOVE GROUND 29000 ksi [ 12000 ksi SHEAR MODULUS] DIAMETER HEIGHT POLE BASE HEIGHT ORIENTATION E-MODULUS

APPURTENANCES

ATTACH POINTS: NO. X, ft 166.00 156.00 146.00 Qty 3 3 3 Description
12' T-Arm 3' Stand-Off
12' T-Arm 3' Stand-Off
12' T-Arm 3' Stand-Off
12' T-Arm 3' Stand-Off
Tri-Collar Mount 30"-36" Pole Di Status Future Appurt Future Appurt Future Appurt 136.00 Future Appurt

Some wind forces may have been derived from full-scale wind tunnel tests.

Pole	Bottom	Thick	Connect	T.A.D	ived fr	om full-	scale wi	nd tunnel	tests.
Section	X,ft. 30.00	<u>in.</u> .18750	Туре	in.	in/ft	ft.	Weight lbs	Steel Spec	Pole
3	128.25	.25000	SLIP-JNT SLIP-JNT	60 <i>.</i> 75.	.2000	53.50 53.50	4907	A572-65	GALVANIZE GALVANIZE GALVANIZE
ECTION P			C-WELD		.2000	47.00	11333	A572-65	GALVANIZE GALVANIZE

Area Ιz IXIY SXSV

X,ft			T, in	Area in²		IxIy in <sup>4</sup>	y sxsy in³		d/t	F <sub>v</sub> (ksi)
84.25 79.25 74.25 64.25 64.25 159.25 147.00 42.75 125 135 175 15 10.75 15 10.75 11 10.75 10.7	3.000 3.	245.6.66.66.22.2.2.2.2.2.2.5.0.0.0.0.0.0.0.0.0.0.0.	.3750 .3750 .3750 .3750 .3750 .37550 .43755 .4375 .4375 .4375 .4375 .4375 .4375	11111111111111111111111111111111111111	2468 24770 334490 24770 3344954 555586 778533784 90110122220 1011174812 20111174812 20111174812 20111174812 2011117481 2011117481 2011117481 2011117481 2011117481 2011117481 20	10385844 113542451 113542451 113542451 113542451 113542451 1135424 1135424 100704668 100704668 100704668 113433157 100704668 113433157 113433157 11343315 113433 113433 113433 113433 113433 113433 113433 113433 113433 113433 113433 113433 113433 113433 113433 113433 113433 113433 113433 11343 113433 113433 113433 11343 113433 113433 11343 11343 113433 11343 11343 11343 11343 11343 11343 11343 11343 11343 11343 1134	8742084857036938708123032773600120464920 879208488570369382892605050505050505050505050505050505050505	25934.73567788899904118.222117.1556778.8899900112.3344.825.545.545.607.888.999.00112.221178.8.999.001111.88999.001111.88999.001.88999.001.88999.001.88999.001.88999.001.88999.001.88999.001.88999.001.88999.001.88999.001.88999.001.88999.001.88999.001.889999999999	0.25.9.25.05.9.9.9.9.9.9.9.3.2.9.5.2.9.5.7.2.8.1.3.6.9.2.5.8.1.3.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0	65.00 TOP 65.00 P01 65.00 P02 65.00 P03 65.00 P03 65.00 Slip-B01

SABRE COMMUNICATIONS COR		
2101 Murray Street		05-Nov-08 15:38 Ph 712.258.6690
Sioux City, IA 51101	Ansonia, CT	Fx 712.258.8250
CASE ~ 1: 3s Gusted Wind		ANSI-TIA-222-G
WIND OLF VERTICAL OLF VERTICAL OLF DESIGN ICE GUST FACTOR (Gh) FORCE COEFF (Cf) IMPORTANCE FAC (I) DIRECTION FAC (Kd) TOPOGRAPHIC CAT	1.00 in EXP-POWER COEFF2  1.10 REFERENCE HEIGHT 900.0  65 PRESSURE @ 32.7 ft 51.8  1.00 BASE ABOVE Grd 1.0  .95 CREST HEIGHT .0	
	Center WEIGHT AREA TX-CAB	Sabre Areas
# Qty Description  1 3 12' T-Arm 3' Stand-Off 9 APXV18-209014-C 3 TMA 2 3 12' T-Arm 3' Stand-Off 12 LPA-185063/8CF 3 3 12' T-Arm 3' Stand-Off 6 7770 6 TMA 6 DIPLEXER 4 1 Tri-Collar Mount 30"-36 3 APXV18-206517-C RESULTS	166.0 5 None 1 156.0 281 40.0 156.0 9 1 5/8" 15	#/Ft Psf Kips Kips Ft-K 73.0 3.84 -1.0 -1.0 1.04 73.0 -4.0 .00 73.0 -0 72.1 2.89 -1.07 1.04 72.1 -3.0 71.1 3.03 -1.08 1.04 71.1 -2.4 .00 71.1 .00 70.1 .8333 1.04 70.0 -1.1
X, ft Kzt psf in 169.00 1.00 47.46 .00 161.00 1.00 47.46 .00 156.00 1.00 46.85 .00 151.00 1.00 46.85 .00 151.00 1.00 46.85 .00 142.75 1.00 45.73 .00 139.00 1.00 45.53 .00 131.00 1.00 45.53 .00 131.00 1.00 45.53 .00 131.00 1.00 44.81 .00 121.00 1.00 44.81 .00 121.00 1.00 44.81 .00 111.00 1.00 44.81 .00 111.00 1.00 43.64 .00 111.00 1.00 42.78 .00 11.00 42.78 .00 11.00 1.00 42.78 .00 11.00 1.00 42.78 .00 11.00 1.00 42.78 .00 11.00 1.00 42.78 .00 11.00 1.00 1.00 1.00 1.00 1.00 1.0	0	Tips
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Z XY-Result X Y36 9.36< 5.54%> -5.89 .00	Z XY-Result .00 5.89

SABRE COMMUNICATIONS CORP JOB: 09-10359 05-Nov-08 15:38 2101 Murray Street Sioux City, IA 51101 BAY STATE DESIGN INC Ph 712.258.6690 Ansonia, CT Fx 712.258.8250 CASE - 2: 3s Gusted Wind 0.9 Dead -🖚 ansi-tia-222-g APPURTENANCES ----Sabre Areas Center WEIGHT AREA TX-CABLE FORCES MOM. Line each each
Elev-Ft Lbs Ft 2 Type Qty #/Ft Psf Kips Kips Ft-K # Qty Description 3 12' T-Arm 3' Stand-Off 9 APXV18-209014-C 166.0 281 52.6 3.84 -.8 -I.O 1 5/8" 18 1.04 None 1 .00 166.0 25 5 73.0 73.0 -3.0 3 TMATMA
12' T-Arm 3' Stand-Off
LPA-185063/8CF
12' T-Arm 3' Stand-Off
7770 166.0 .0 -.8 156.0 281 40.0 281 42.6 35 1 5/8" 15 1.04 None 1 .00 72.1 2.89 - .7 156.0 72.1 -2.3 3 12' T-Arm 3' Stand-Off 146.0 281 42.6 7770 71.1 146.0 35 1 5/8" 12 1.04 71.1 146.0 5 None 1 .00 71.1 146.0 146.0 5 None 1 .00 71.1 146.0 3.03 -.8 . 0 .83 -.2 ~ . 3 RESULTS -| ShearX ShearY AxiaZ | BendX BendY TorqZ | .0 .00 -.1 .0 .0 .0 MIND ICE F'y Inter ksi 4.8.2 psf 47.64 47.46 47.16 X, ft 169.00 Kzt in 1.00 .00 .0 .00 .0 4.62 .0 5.29 .0 9.01 -1.4 -25.2 -52.4 -97.4 -.1 -3.6 . 0 .0 .000 65.00 166.00 1.00 .00 , ŏ 65.00 65.00 . 0 .008 161.00 .ŏŏ .0 1.00 -3.8 ٠Ò . 0 .059 156.00 1.00 46.85 .00 -6.8 .0 151.00 . 0 .113 46.53 .00 9.56 -7.1 -9.7 . 0 65.00 .189 146.00 1.00 46.21 .00 13.30 13.71 14.11 -146.0 -189.2 , Ó 64.63 63.98 .0 45.99 45.73 45.53 45.17 142.75 .264 .00 . 0 -10.1 .328 139.00 1.00 -10.5 -11.9 .00 -240.6 -283.2 65.00 .300 136.00 1.00 .00 15.51 65.00 .339 131.00 1.00 .00 . 0 -12.3 -12.7 16.10 -360.8 . 0 65.00 16.10 16.70 17.30 17.92 18.54 19.17 .403 126.00 1.00 44.81 . 0 -441.3 -524.8 65.00 .461 .00 121.00 1.00 44.43 . 0 -13.2 -13.7.0 65.00 116.00 -611.3 -700.8 -793.5 -889.2 1.00 44.04 iõõ . 0 . Q 65.00 .564 111.00 1.00 43.64 43.22 42.78 .00 ٠Ŏ -14.2 -14.7 . 0 65.00 .609 106.00 1.00 .00 .0 65.00 .651 101.00 .00 , ŏ -15.2 -15.6 .690 .731 96.00 42.33 42.17 1.00 .00 ٠Õ 20.24 64.56 64.30 -988.3 94.25 1.00 -1023.3 -1127.5 .00 . 0 -16.4 1.00 .746 89.25 41.70 .00 21.39 -17.6-1127.5 65.00 65.00 .0 .533 84.25 22.08 22.76 23.44 41.20 .00 -18.6 -1234.2 79.25 1.00 40.68 .00 65.00 65.00 -19.4-1344.2 74.25 69.25 1.00 40.13 .00 -20.2 -1458.3 -1575.8 .593 1.00 .00 24.12 -21.1 65.00 .611 1.00 38.94 -15/5.8 -1695.8 -1820.0 -1947.5 -2078.3 64.25 24.81 25.49 .00 -21.9 65.00 .628 59.25 1.00 38.30 .00 -22.8 54.25 49.25 65.00 .644 1.00 37.60 .00 . 0 26.17 -23.8 65.00 1.00 .659 36.86 .00 26.67 27.16 27.59 47.00 65.00 36.51 35.67 .00 -2138.3 -2274.2 -25.6 65.00 65.00 42.00 .680 .00 -26.5 -27.5 40.75 ī.ŏŏ .615 35.45 28.01 .00 -2309.2 -2449.2 -2592.5 -2739.2 .618 1.00 -28.9 34.51 .00 28.67 30.75 25.75 20.75 65.00 1.00 .629 33.46 32.28 .00 29.31 -30.0 65.00 1.00 .639 .00 29.96 -31.2 65.00 .649 1.00 30.90 .00 30.62 -32.4 -2888.3 -3041.7 -3198.3 65.00 .658 15.75 1.00 29.25 .00 . 0 31.29 -33.6 65.00 .667 10.75 1.00 28.62 .00 . 0 31.97 -34.8 65.00 65.00 65.00 .675 5.75 1.00 28.62 .00 -3358.3 -3521.7 . 0 32.65 -36.1 .683 1.00 .00 28.62 .0 33.05 -36.8 ,690 .00 1.00 28.62 - 0 .00 33.10 -36.9 3545.8 65.00 .691 DISPLACEMENTS -

SABRE CON	MUNIC	CATIONS	CORI	•	J	OB: 09	-10359		05-	Nov-08 1	5:38
2101 Murr Sioux Cit	zay St Zy, IA	reet 4 51101			BAY :	STATE 1	DESIGN IN	IC	Ph	712.258.	6690
CASE - 3:						Ansoni	a, CT			712.258.	
•									<u>A</u> 1	SI-TIA-2	22-G
VEI DES	RTICAL	OLF		1.00	GUS? EXP-	TED WIND CAT/STR	(3sec) RUC CLASS	50.0 m	mph 80	.5 kph	
GUS FOR	ST FAC	CTOR (	Gh)	.75 ir.	EXP- REFE	POWER C	OEFF. EIGHT	900.0 f	)5 F#		
ĬMI DTR	PORTANO	E FAC	I)	1.00	PRES BASE	SURE @ Above	32.7 ft Grd	6.7 p	sf 320	.0 Pa	
TOI	POGRAPI	IIC CAT	κα <i>)</i>	. 95 1	CRES	T HEIGH	O (3sec) RUC CLASS COEFF. BEIGHT O 32.7 ft Grd	.0 f	t		
THE COLLEGE	CES				<b>7</b>					-Sabre A	ceas
# Qty Des	cripti	on			Center Line Elev-F	WEIGHT each	' AREA each	Tx-CABLE	E Wini	FORCES	MOM.
יי ו 1 3 12 ייי	'- Drm 2	1 64004	OFF					- 7-7 #	YFC PSI	Kips Kip	s Ft-K
1 3 12' T 9 APX 3 TMA 2 3 12' T 12 LPA 3 3 12' T 6 TMA 6 DIP	V18-20	9014-C	V-1		166. 166.	0 309 0 64	66.3	8" 18 1	9.4 9.4 9.4	.63 ~1. ~6. .49 ~1. ~5. .53 ~1. ~3. ~3. ~1.	82 3
_ 2 3 12' T	'-Arm 3 -18506	' Stand- 3/8CF	-Off		156.	0 309	52.5 None	1	.00 9.4 9.3	 49 -1.	3 71
- 3 3 12' T	'-Arm 3 0	' Stand-	-Off		146.	0 309	57.6	B" 15 1	9.3	-5. .53 -1.	0 B1
6 7MA 6 DIP: 4 1 Tri-C	LEXER				146.	0 15 0 15	None	1 1	.00 9.2	-3. 	7 5
- 4 1 TF1-U	011ar V18-20	Mount 30 6517-Ç	"-36"	Pole D	i 136. 136.	0 279 0 52	16.7	T 211 & 1	9.0	.15	5 3 1
RESULTS											7
X, ft 169.00	Kzt 1.00	bat MIND	ICE in	Shear	FORCES, I	kips CY Axia?	-:MOMENT	S,ft-kij	ps:	F'y Inter ksi 4.8.2	
166.00	1.00	11.36 $11.32$	1.77	Shear	.01	2 -8.3	BendX -10.1 -10.1 -30.5 -39.6 -76.2 -74.2 -112.8 -74.3 -151.8 -172.6 -194.0 -216.3 -214.8	.0	.0 6	5.00 .000 5.00 .010	
156.00 151.00	1.00	11.17	1.75	.0	1.11	-8.9 -15.6	-5.1 $-10.7$	.0	.0 6	5.00 .021 5.00 .038	
146.00 142.75	1.00	11.02	1.74	.0	2.82	-16.2 -22.7	-20.1 -30.5	. 0	.0 6	5.00 .054 4.63 .076	
139.00 136.00	1.00	10.90	1.73	.0	3.04	-23.4 -24.2 -27.0	-39.6 -50.6	.0	.0 6	3.98 .090 5.00 .079	
131.00 126.00	$1.00 \\ 1.00$	10.77 10.68	1.72	. 0	3.52	-27.8	-59.8 -76.6	.0	.0 6	5.00 .089 5.00 .103	
116.00	1.00 1.00	10.59 10.50	$\frac{1.71}{1.70}$	. 0	3.84 3.99	-29.6	-112.6	. 0	.0 6	5.00 .116 5.00 .128	
106.00	1.00	10.40 $10.30$	1.69	. ŏ	4.15	-31.5	-151.8	.0	.0 6	5.00 .139 5.00 .149	
96.00	1.00	10.20 10.09	1.68	. ŏ	4.47 4.58 4.69	-33.5	-194.0	.0	.0 6	5.00 .159 5.00 .168	
89.25		2.24	1.67	. 0	4.69	-35.5 -37.4	-224.3	.0	.0 64	1.56 .178 1.30 .182	
79.25	1.00	9.82 9.70 9.57	$1.65 \\ 1.64$	. 0	5.04 5.21	-39.0 -40.4	-272.2	. 0	,0 69	5.00 .135	
69.25	1.00	9.43	1.63 1.62	. 0	5.38 5.54	-41.9 -43.4	-297.3 -323.3 -350.3	.0	.0 65	5.00 .140 5.00 144	
59.25	1.00	9.28 9.13	1.61 1.59	. ŏ	5.71 5.87	-44.9 -46.4	-377.9 -406.5	.0	.0 65	.00 .149 .00 .153	
49.25	1.00	8.79	1.58 1.56	. 0	6.04	-48.0 -49.3	-435.8 -466.0	.0	.0 65	.00 .157 .00 .161	
42.00	1.00	8.70 8.50	1.56 1.54	. 0 . 0	6.15 6.27 6.37	-50.9 -52.4	-479.9 -511.3	. 0 . 0 . 0	.0 65	.00 .164	
35.75 1	1.00	8.23	1.54 1.52	. 0 . 0	6.47	-54.0 -56.2	-519.2 -551.6	. 0	.0 65	.00 .150	
25.75	1.00	7.70	1.49	. 0 . 0	6.78 6.93	-58.1 -60.0	~584.7 ~618.6	.0	.0 65	.00 .154	
15.75 1	L.00 L.00	6.97	1.44	.0	7.08 7.23	-61.9 -63.9	-653.2 -688.6	. 0	.0 65	.00 .159 .00 .162	
5.75 1	L.00 L.00 L.00	6.82 6.82	1.35	.0	7.38 7.53	-65.9 -67.9	~724.8 ~761.6	.0	.0 65	.00 .164 .00 .166 .00 .168	
.00 1	.00		1.12 1.06	.0	7.62 7.63	-69.1 -69.2	-799.3 805.0	.0	.0 65	.00 .168 .00 .170 .00 .170	
DISPLACEME ELEV	ents		FT,R.Cart	ON feet			·				
X, ft 169.00	X .00	Y		z	XY-Res	ult '	X	-ROTATIO	ON, degr	eesXY-Result	
		_,,		- 44	2.04< 1	·- 4 T & >	-1.27	.00	.00	1.27	

2101 Murray Sioux City, CASE - 4: Se:	Street IA 51101	P JOB: 09-10359 BAY STATE DESIGN INC Ansonia, CT	05-Nov-08 15:38 Ph 712.258.6690 Fx 712.258.8250
WIND VERTICA DESIGN GUST FORCE C IMPORTA DIRECTI TOPOGRA	OLF AL OLF ICE FACTOR (Gh) COEFF (Cf) NCE FAC (I) ON FAC (Kd) PHIC CAT	1.00 GUSTED WIND (3sec) 60.0 m 1.00 EXP-CAT/STRUC CLASS C-II 1.10 REFERENCE HEIGHT 900.0 f 1.00 BASE ABOVE Grd 1.0 1.00 CREST HEIGHT .0 f	ANSI-TIA-222-G  Aph 96.6 kph  5 t sf 412.3 Pa
# Qty Descrip  1 3 12 T-Arm 9 APXV18-2 3 TMA 2 3 12 T-Arm 12 LPA-1850	tion  3' Stand-Off  209014-C  3' Stand-Off  063/8CF 3' Stand-Off  the stand-Off  Mount 30"-36"  06517-C	Center WEIGHT AREA TX-CABLE Line each each Elev-Ft Lbs Ft 2 Type Qty #/  166.0 281 52.6 166.0 25 1 5/8" 18 1. 156.0 281 40.0 156.0 281 42.6 146.0 35 146.0 35 146.0 5 15/8" 12 1. 146.0 5 None 1 . Pole Di 136.0 254 11.9	Sabre Areas   FORCES   MOM.
X,9.000 1.00	WIND DSF .000 .000 .000 .000 .000 .000 .000 .0	FORCES, kips	SorqZ    Ksi   4.8.2   0.000   0.006   0.000

SABRE COMMUNICATIONS CORP JOB: 09-10359 05-Nov-08 15:38 2101 Murray Street BAY STATE DESIGN INC Sioux City, IA 51101 Ph 712.258.6690 Ansonia, CT Fx 712.258.8250 SHAPE: 18 SIDED POLYGON with FLAT-FLAT ORIENTATION BOLTS: QUADRANT SPACED BOLTS 6.00 in. ON CENTER LOCATE: POLE DATA 56.18 in. .4375 in. .2000 in/ft 65.00 ksi DIAMETER = -48.8 kips Vert 21.1 kips Long 25.5 kips Tran 2539.3 ft-kips Tran 2539.3 ft-kips Long .0 ft-kips Vert BASE AXIAL FORCE= SHEAR X = SHEAR Y = PLATE ₹ ACTIONS = TAPER ≈ POLE Fy ≈ X-AXIS MOM = Y-Axis MOM = Z-Axis MOM = DESIGN CASE = 1 3s Gusted Wind -Design: ANY Orientation Reactions at 45.00 deg to X-AXIS BOLT LOADS AXIAL - COMPRESSION AXIAL - TENSION = 174.76 kips= 168.66 kips SHEAR 2.91 kips = 2.91 kips = 3.77 ksi = .95 ksi = 75.00 ksi = 100.00 ksi AXIAL STRESS SHEAR STRESS YIELD ULT. STRENGTH Fy STRENGTH Fu Interaction ALLOW Fa [ .80 x 1.00] = Fv [ .80 x .40] = STRESS 80.00 ksi .696 TIA-G SHEAR 32.00 ksi TENSION AREA REQUIRED 2.18 in^2 3.25 in^2 3.07 in^2 TENSION AREA FURNISHED = AREA FURNISHED A615 ::: ANCHOR BOLT DESIGN USED 16 Bolts on a 62.750 in. Bolt Circle SHIP 2.250 in. Diameter 67.13 in. Embedded (lbs) 12.00 in. Exposed 84.00 in. Total Length 2185 CONCRETE - Fc= 4000 psi ANCHOR BOLTS are STRAIGHT w\ UPLIFT NUT BASE PLATE . [Bend Model:

Flat~ 17] TH = 60.0 ksi TH = 30.6 in. = 1670.0 in.k EQD = 2.463 in. ESS = 36.4 ksi ESS = 54.0 ksi .90 x 1.00] YIELD STRENGTH BEND LINE WIDTH = PLATE MOMENT =
THICKNESS REOD =
BENDING STRESS =
ALLOWABLE STRESS = [Fy x

	BAS	E PLATE USED	
3.00	in.	THICK	SHIP
61.25	in.	SQUARE	(lbs)
		CENTER HOLE	1654
12.00	in.	CORNER CLIP	

### LOAD CASE SUMMARY -

	ETC)	2000 A.	•				ABol	t-Str	Plate-	str	
<sub>T.C</sub>	FORCES-(kips) LC Axial ShearX ShearY			MOMENTS-(ft-k)				Allow _Actual Allow Des			Design
1	48.8	SHEALY			Y-axis	TorQ		ksi	ksi	ksi	Code
61	36.9	21.1	25 <b>.5</b>	2285	2770	0	. 696	75.00	36.41	54.00	TIA-G
2		21.1	25.5	2256	2735	0	.685	75.00	35.79	54 00	TTN-C
13	69.2	4.9	5.9	512	621			75.00			TIA-G
4	39.7	3.5	4.3	378	458	0		75.00		54.00	